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ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-41G) LAUNCH

By D. L. Johnson, C. K. Hill, G. Jasper and G. W. Batts
Systems Dynamics Laboratory

November 1984





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This report presents a summary of selected atmospheric conditions observed near Space Shuttle STS-41G launch time on October 5, 1984, at Kennedy Space Center Florida. Values of ambient pressure, temperature, moisture, ground winds, visual observations (cloud), and winds aloft are included. The sequence of prelaunch Jimsphere measured vertical wind profiles is given in this report. The final atmospheric tape, which consists of wind and thermodynamic parameters versus altitude, for STS-41G vehicle ascent has been constructed. The STS-41G ascent atmospheric data tape has been constructed by Marshall Space Flight Center's Atmospheric Sciences Division to provide an internally consistent data set for use in post flight performance assessments.

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TABLE OF CONTENTS

		Page
I.	INTRODUCTION	1
II.	SOURCES OF DATA	1
ш.	GENERAL SYNOPTIC SITUATION AT LAUNCH TIME	1
IV.	SURFACE OBSERVATIONS AT LAUNCH TIME	2
v.	UPPER AIR MEASUREMENTS DURING LAUNCH	2
	A. Wind Speed B. Wind Direction C. Prelaunch/Launch Wind Profiles D. Thermodynamic Data E. SRB Upper Air and Surface Measurements	2 3 3
REFE	CRENCES	35

LIST OF ILLUSTRATIONS

Figure	Title	Page
1.	Surface synoptic chart 57 min after launch of STS-41G	25
2.	500 mb map 57 min after launch of STS-41G	26
3.	GOES-5 visible imagery of cloud cover 3 min prior to launch of STS-41G (1100 UT, October 5, 1984). 500-mb contours and wind barbs are also included for 1200 UT	27
4.	Enlarged view of GOES-5 visible imagery of cloud cover taken 3 min prior to launch of STS-41G (1100 UT, October 5, 1984). Surface temperatures and wind barbs for 1100 UT are also included	28
5.	Scalar wind speed and direction at launch time of STS-41G	29
6.	STS-41G prelaunch/launch Jimspehre-measured wind speeds (FPS)	30
7.	STS-41G prelaunch/launch Jimspehre-measured wind directions (degrees)	31
8.	STS-41G prelaunch/launch Jimsphere-measured in-plane component winds (FPS). Flight azimuth = 39 degrees	32
9.	STS-41G prelaunch/launch Jimsphere-measured out-of-plane component winds (FPS). Flight azimuth = 39 degrees	33
10.	STS-41G temperature profiles versus altitude for launch (ascent)	34



LIST OF TABLES

Fable	Title	Page
1.	Selected Atmospheric Observations for the Flight Tests of the Space Shuttle Vehicles	4
2.	Systems Used to Measure Upper Air Wind Data for STS-41G Ascent	5
3.	Surface Observations at STS-41G Launch Time	6
4.	STS-41G Pre-Launch Through Launch KSC Pad 39A Atmospheric Measurements	7
5.	STS-41G Ascent Atmospheric Data Tape	8

TECHNICAL MEMORANDUM

ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-41G) LAUNCH

I. INTRODUCTION

This report presents an evaluation of the atmospheric environmental data taken during the launch of the Space Shuttle/STS-41G vehicle. This Space Shuttle vehicle was launched from Pad 39A at Kennedy Space Center (KSC), Florida, on a bearing of 39 deg east of north at 1103 UT (0703 EDT) on October 5, 1984.

This report presents a summary of the atmospheric environment at launch time (L+0) of the STS-41G, together with the sequence of prelaunch Jimsphere measured winds aloft profiles from L-12 hr through liftoff. The general atmospheric situation for the launch and flight area is described, and surface and upper level wind/thermodynamic observations near launch time are given. Since the ship Redstone was unavailable for STS-41G duty, the SRB descent/impact atmospheric data were not taken. However, one can use the STS-41G ascent data for SRB studies, as the best substitute.

Previous MSFC-related launch vehicle atmospheric environmental conditions have been published as Appendix A of individual MSFC Saturn Flight Evaluation Working Group reports [1]. Office memorandums have been issued for previous flights giving launch pad wind information. A report has also been published [2] which summarizes most launch atmospheric conditions observed for the past 155 MSFC/ABMA-related vehicle launches through SA-208 (Skylab 4). Reports summarizing ASTP, STS-1 through STS-41D launch conditions are presented in References 3 through 15, respectively. Table 1 gives the atmospheric L+0 launch conditions for all the Space Shuttle missions.

II. SOURCES OF DATA

Atmospheric observational data used in this report were taken from synoptic maps made by the National Weather Service, plus all available surface observations and measurements from around the launch area. Upper air observations were taken from balloon-released instruments sent aloft from Cape Canaveral Air Force Station (CCAFS). High-altitude winds and thermodynamic data were measured by the Super-Loki rocketsondes launched from the CCAFS. Table 2 presents a listing of systems used to obtain the upper level wind profiles used in compiling the final ascent atmospheric data tape. Data cutoff altitudes are also given in Table 2.

III. GENERAL SYNOPTIC SITUATION AT LAUNCH TIME

An area of high pressure, located in the Atlantic just off the Virginia coast, prevailed over the southeastern states just prior to STS-41G liftoff. This air mass brought warm and less humid conditions to the KSC area throughout the countdown period. Light to moderate northeast to easterly surface winds were the rule during

countdown. Figure 1 presents the surface map conditions approximately 57 minutes after launch. Figure 2 depicts the winds aloft conditions at the 500 mb pressure level approximately 57 minutes after launch. Westerly winds dominated the flow aloft over the KSC Florida area. Skies were mostly scattered to broken throughout the early morning of October 5, 1984. Figure 3 presents the GOES-5 visible picture taken at 1100 UT (3 minutes before liftoff). Figure 4 shows an up-close visible shot of the Florida peninsula as recorded by GOES-5, taken also at 1100 UT.

IV. SURFACE OBSERVATIONS AT LAUNCH TIME

Surface observations at launch time for selected KSC locations are given in Table 3. Included are pad 39A, shuttle runway, and CCAFS balloon release station observations. Neither precipitation nor lightning was observed at launch time.

Table 4 presents Pad 39A wind data along with other standard hourly atmospheric measurements and sky observations for the 6-hr period prior to launch of STS-41G. Values for wind speed and direction are given for the 84 m (275 ft) FSS reference level and 18 m (60 ft) pad light pole level.

V. UPPER AIR MEASUREMENTS DURING LAUNCH

The FPS-16 Jimsphere (1118 UT), MSS Rawinsonde (1106 UT), Super-Loki Rocketsonde (1403 UT), and Super-Loki Robin (1207 UT) systems were used to measure the upper level wind and thermodynamic parameters for STS-41G launch. At altitudes above the rocket-measured data, the Global Reference Atmosphere (GRA) [16] parameters for October KSC conditions were used. A tabulation of the STS-41G final atmospheric data for ascent is presented in Table 5 which lists the wind and thermodynamic parameters versus altitude. A brief summary of parameters is given in the following paragraphs.

A. Wind Speed

At launch time, wind speeds were $16.5 \, \text{ft/sec}$ (9.8 kn) at 60 ft and increased to a maximum of 78 ft/sec (46 kn) flowing from 303 deg. This maximum occurred at an altitude of $40,600 \, \text{ft}$ (12,375 m). The winds decreased above this level as shown in Figure 5. The overall maximum measured speed was 133 ft/sec (79 kn) at 247,000 ft (75,286 m) altitude.

B. Wind Direction

At launch time, the 60-ft wind direction was from the east northeast (73 deg) and shifted through east and south into a west northwesterly component above 32,000 ft (9754 m). Winds remained westerly through 66,000 ft (20,117 m) altitude. Winds above this level shifted into an easterly component, but oscillated enormously above 132,000 ft (40,234 m) as shown in Figure 5. Figure 5 shows the complete wind direction versus altitude profile, which indicates the wind direction became quite variable at altitudes with low wind speeds.

C. Prelaunch/Launch Wind Profiles

Prelaunch/launch wind profiles presented in Figures 6 through 9 were measured by the Jimsphere FPS-16 system. Data are shown for four measurement periods beginning at L-12 hr and extending through L+0.

The wind speed and direction profiles for the 12-hr period prior to and including L+0 are shown in Figures 6 and 7. The in-plane (head-tail wind) and out-of-plane (left-right crosswind) profiles are given on Figures 8 and 9. There were no calculated vehicle load exceedances produced by the wind data presented. The prelaunch atmospheric conditions are discussed in more detail in Section III.

D. Thermodynamic Data

The thermodynamic data taken at STS-41G launch time, consisting of atmospheric temperature, dew-point temperature, pressure, and density have been compiled as the STS-41G ascent atmospheric data and are presented in Table 4. The vertical structure of temperature and dew-point temperature for the STS-41G ascent are shown graphically versus altitude in Figure 10.

The atmospheric thermodynamic parameters of temperature, pressure, and density, measured during STS-41G launch below 102,000 ft (31,090 m) were all within 2 percent of their respective PRA-63 [17] annual values. All these parameters stayed within 20 percent of their respective PRA-63 values, at all levels of measurement.

E. SRB Upper Air and Surface Measurements

As has been mentioned in the introduction, since there was no ship available, an SRB descent atmospheric data tape has not been constructed. The tabular values for the ascent atmospheric tape as presented in Table 5 should be used for SRB descent/impact studies since it is the closest measured data source.

SELECTED ATMOSPHERIC OBSERVATIONS FOR THE FLIGHT TESTS OF THE SPACE SHUTTLE VEHICLES TABLE 1.

1. 1. 1.

,						Surface (Surface Observations	ons		քույսլ	Inflight Conditions	ons	
	>	Vehicle Data	<i>æ</i>		Thermo	Thermodynamic ^a		Windb	q	Ma Belo	Max. Wind Below 60,000	٤	Count Down
	Vehicle No.	Launch Date	Time (EST) Nearest Minute	Launch Pad	Press. ^c N/cm ²	Temp.	Rel. Hum. (8)	Speed (ft/sec)	Dir. (deg)	Alt.	Speed (ft/sec)	Dir. (deg)	Launch Comments of Veteorological Significance
STS-1 Columb	STS-1 Columbia	4/12/81	0400	39A	10.234 ^d	1.5	95	11.8	125 120	44.300	86	250	
STS-2 Columb	STS-2 Columbia	11/12/81	1010	39A	10.166	53	19	27.0	345 355	36, 300	158	786	
STS-3 Columb	STS-3 Columbia	3/22/82	1100	39A	10.160	र त	7.1	9.0e	50e 145e	45.000	611	750	Wind directional change observed at Pad just prior to L-10. Onser of sea breeze.
STS-4 Columb	STS-4 Columbia	6/27/82	1100 ^f	39A	10.200	6.7	. 0.	5.88 4.98	133 ^g 141 ^g	47.900	37	329	
STS-5 Columb	STS-5 Columbia	11/11/82	0719	39A	10.227	22	89	22.0 35.0	8 8	40,600	146	336	
STS-6 Challer	STS-6 Challenger	4/4,83	1330	39A	10.183	23	55	12.7	63 55	46,100	155	277	
STS-7 Challer	STS-7 Challenger	6/18/83	0733 ^f	39A	10.146	52	80	$\frac{5.9^{e}}{10.3^{e}}$	$\frac{10^{\mathrm{e}}}{350^{\mathrm{e}}}$	45.900	92	278	
STS-8 Challer	STS-8 Challenger	8/30/83	0232 ^f	39A	10.111	24	97	8.8 14.0	269 268	45,100	30	349	17 min countdown delay due to adverse weather conditions.
STS-9 (SL-1) Columb	STS-9 (SL-1) Columbia	11/28/83	1100	39A	10.153	24	83	19.1 32.0	183	47,100	117	252	Thunderstorms in area.
STS-11 (41-B) Challen	STS-11 (41-B) Challenger	2/3/84	0080	39A	10.173	17	75	0.0 NA	o V	38.200	143	1988	
STS-13 (41-C) Challen	STS-13 (41-C) Challenger	4/6/84	0858	39A	10.149	16	99	21.5 18.6	320 275	37,700	921	289	
4 ×	STS-41D Discovery	8/30/84	0842 ^f	39A	10.172	26	81	3.0	106 39	40.300	44	270	
STS-41G Challeng	STS-41G Challenger	10/5/84	0703 ^f	39A	10.210	23	09	16.5 14.8	7.3 5.8	40.600	%- 	303	

Pad 39A thermodynamic measurements taken at approximately 1.2 m (4 ft) above natural grade at camera site No. 3. 1 min average prior to L+0 of 60 ft PLP (listed first) and 275 ft FSS winds measured above natural grade. Pressure measurement applicable to 21 ft above MSL unless otherwise indicated. Pressure measurement applicable to 14 ft above MSL. Bestern Daylight Time. 30 sec average prior to L+0.

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TABLE 2. SYSTEMS USED TO MEASURE UPPER AIR WIND DATA FOR STS-41G ASCENT

	Date: October 5, 1984	ber 5,		Portion of Data Used	Data Used	
	Release Time	Time	Start		Fnd	þ
Type of Data	Time (UT) (hr/min)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)
FPS-16 Jimsphere	11:18	15	6 (21)	15	17,069 (56,000)	14
MSS Rawinsonde	11:06	က	17,373 (57,000)	09	28,346 (93,000)	96
Super-Loki Rocketsonde (Datasonde)	14:03	180	40,843 (134,000)	180	28,651 (94,000)	193
Super-Loki Rocketsonde (Robin)	12:07	64	83,515 (274,000)	64	41,148 (135,000)	65

TABLE 3. SURFACE OBSERVATIONS AT STS-41G LAUNCH TIME

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							Sk	Sky Cover		Wind	pı
Location ⁸	Time After L+0 (min)	Pressure (MSL) N/cm ² (psia)	Temperature °K (°F)	Dew Point °K I	Relative Humidity (%)	Visibility km (miles)	Cloud Amount**	Cloud	Height of Base Meters (ft)	Speed ft/sec (kt)	Direction (deg)
NASA Space Shuttle Runway X68e Winds Measured at 10.4 m (34 ft)	0	10.217 (14,819)	292.9 (67.5)	288.7 (60.0)	92	16 (10)	3 2	Strato- cumulus Cirrus	1158 (3800) 10,058 (33,000)	3.4 (2.0)	20
CCAFS XMR ^C Surface Measurements	÷	10.213	291.5 (65.0)	287.6 (58.0)	78	13 (8)	ဟ က	Strato- cumulus Cirrus	1524 (5000) 10,363 (34000)	3.4 (2.0)	06
Pad 39A ^d Lightpole SE 18.3 m (60.0 ft)	0	10.210* (14.808*)	296.5 (74.0)	288.2 (59.0)	09	ı	ŀ	ı		16.5 ^b	73 ^b
Pad 39A FSS (Top SE) 83.8 m (275 ft)	0	1	-	ı	1	ı	1	_		14.8 ^b (8.8)	58 ^b

*Pad 39A Camera Site 3 barometric pressure instrument appeared to be reading too high. Therefore, the KSC Shuttle runway station pressure value interpolated to 10.210 N/cm² at 21 ft above MSL was used as the L+0 pad atmospheric pressure measurement. Sea level pressure was 10.217 N/cm².

**7/10 total sky cover reported at both X68 and XMR.

- a. Altitudes of measurements are above natural grade, except where noted.
- Approximately 1 min average prior to L+0.
- Balloon release site.
- Pad 35A thermodynamic measurements are taken at camera site No. 3, approximately 6.4 m (21 ft) above MS. Ď.
- official STS-41G sky observational site.

TABLE 4. STS-41G PRE-LAUNCH THROUGH LAUNCH KSC PAD 39A ATMOSPHERIC MEASUREMENTS⁸

18

		irks								
		Other Remarks	_							
		Vis.	21	10	10	10	10	10	10	10
oup	Total	Sky Cover	6/10	7/10	4/10	5/16	9/10	8/10	5/16	7/10
Sky Ccndition ^b		Clouds	Broken at 4500 ft	Broken at 4200 ft	Scattered at 4200 and 10,000 ft	Scattered at 3800 ft	Broken at 3800 ft	Broken at 3800 ft	Scattered at 3800 and 33,000 ft	5/10 SC at 3800 ft 3/10 CI at 33,000 ft
	evel	WD°	108	095	094	076	117	680	0 6 6	073
	60' Level (SE)	WS Kt	11	6	۲	12		x o	10	10
ents	evel)	WDo	100	060	220	071	106	880	048	058
asureme	275' Level (SE)	WS Kt	10	10	9	11	6	∞	10	6
ric Me		8. 8.	23	26	61	57	52	54	09	99
tmosphe		(°F)	51	25	59	28	55	26	9	59
Hourly Atmospheric Measurements	f	(°F)	73	73	73	7.4	74	74	74	74
H	f Ootobox 1004	Time UT	0200	0090	0040	0800	0060	1000	1100	L+0 ^c 1103

Hourly pad observations (obtained via MSFC/HOSC) averaged over 1 min, centered on the hour.

b. Sky observations taken at the Shuttle runway site X68.

L+0 PAD Wind and thermodynamic parameters obtained from HOSC strip charts. SE Anemometers used at 60 and 275 ft levels for L+0 wind conditions (approximately 1 min average prior to L+0). Pad 39A L+0 atmospheric pressure, at 21 ft (MSL), was 10.210 N/cm². Sea level pressure was

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TABLE 5. STS-41G ASCENT ATMOSPHERIC DATA TAPE

ALTITUDE	LING SPEED	HIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	DE N. POLINT
(FT)	(FT/SEC)	(DE 6.)	(DEG C)	(MILLIBARS)	(GRAN/HS)	(086 C)
120203	303	Jea	2343	*1021+C#	1192154	1545
C001CG	C16	010	23.1	.1018+34	.1193-64	15.0
	615	065	- 23.6	-1015+04	1186+nu	15.0
200320	614	C66	22.6	*C+1101.	.1163+94	14.9
20000		086	2	+1007+3#		14.9
20020	Č13	786	22.4	*10+7CUT*	.1176+C4	14.9
:00400:	015	374	٠.	40470014	474774	16.9
001303	019	065	12.0	.9969+03	.1169+F4	14.9
200800	213	09 th	21.6	-0934-63	.1166+24	14.8
-3600D	910	1 60	21.6	€0+6696•	.1162+C4	14.8
201033	C15	080		9665+03		14.6
201105	C18	060	21.1	*9830+0≅	.1156+74	14.6
מיבוסי	013	DA6	de:2	A9795+GI	1159.54	1441
C0133C	019	060	20.5	.9761+03	.1151+04	14-1
0.812.	613	060	26.2	.9726+CI	-1148+C4	13.9
001500	617	16.2	0.00	.9692+03	*1148+14	13.7
014.00	617	29.2	•	29 4 5 ± 5 £ 2	1162+Cu	13.4
691700	750	160		9624+03	1149+04	13.2
- F1833	022	DAS	1901	.9550.	41137+04	13.0
531963	021	603	18.7	.9556+03	.1134+04	12.7
Cozeaa	021	08.0	14.4	.9523+03	.1131+04	12.5
502130	C13	200	18.2	.9489+63	.1128+P4	12.4
0022-0	120	660	17.9	9455+03	.1125+C9	12.3
002339	621	160	17.7	.9422+03	-1122+54	12.2
552955	ñzu	695	17.4	.9396+C3	1119-04	12,1
002520	025	103	17.2	*9355+OE	.1116+P4	12.3
C026CE	021	131	17°	.9322±£3	1113+04	11.8
2027.7	220	# OC -	16.7	.9289+03	30+0414	11.7
JE29Jr	924	29.5	10.5	◆9256+03	*2*1011*	Ileb
_02927	622	66L	(2) 9 :	10 + M < N < N < N < N < N < N < N < N < N <	30+30HH.	11.5
בניטניטנ	021	760	1441	49192403	1101+04	#all
203100	E 123	M of	15.7	.9157+03	10 + 86 CH +	3
2032.0	623	ברז	15.5	-9124+EI	#1:95+24	1104
C03300	1:0	159	15.2	.9092+03	# 1 + 2 6 C T •	***
C3343C	621	260	. ₹ 5•₽	-9059+02	* 1089+04	11.4
003501	023	360	14.7	.9027-03	*1.386+1.	11.4
256.0	222	163	4444	10+408*	, 1083+24	1104
SF 37 2	020	101	14.2	•89€2+€3	\$0.40 % °	11.4
223963		292	13.9		.1277+54	11.4
503853	a.c.	663	13.7	PO+0000•	1175+Jt	11.4
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いつかきのい	619	116	¥•11	.87.77+03	#U+85LL*	8.0
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TABLE 5. (Continued)

	(FT/SEC)	(050)	(DEG C)	(HILLIBARS)	(GRAN/H3)	(0 930)
1	025	116	16.4	.8550+01	41065+A4	1401
	220	K) v	M • D = 0	.8519+03	.1542+04	9.3
ì	070	411	15.2	.8488+03	.1038+D%	Bab
	3 6	071	- C	-8457+03	*1035+C4	7.0
1	910	113	nent	20403	*153Z+04	200
	018	0	P 0	00+040 00	1024-04	
	017	111	0	0.7.24.0.7	10210	4:
- 1	016	09.1	0 v	10 +4C + 4C	ACADADA	
	019	- C	3.0	-A271407	1014 + 04	202
J.	021	Da6	200	18763-03	10 10 10 10 10 10 10 10 10 10 10 10 10 1	4.6
	010	089	9.6	.8213+03	-1009+D#	9-1
ı	018	284	8.6	M 0 + 4 C T C T	40+401	
	020	085	10.3	8154+03	100000	3
- 1	919	160	1004	4125+01	FC+0400	
	016	960	0.00 0.00	.8095+03	10+1000	7.10
- 1	817	080	11.2	80+63	10+4540	27.5
	018	7 60		.8037+03	9812+01	17.
	01.2	162	11.9	.8667+03	2747403	
	615	09.8	12.2	.7978+03	-9722+01	2.4
	016	960	12.5	70504	10477401	
	016	101	12.3	.7921+03	EC+6896"	-5.0
	C13	112	12.1	7862+03	-9622+03	
	C11	C9 B	11.00	.7863+C3	.0594+73	-6.2
	012	09.6	11.6	.7835aE3	49567403	-6. I
	600	102	11.4	.7806+63	.9539+03	4.9-
	700	080	11.2	.7778+03	49512+93	2445
	6 00	960	11.0	.7756+03	•9485+33	9-9-
	900		1201	-7721+63	- 9458+T	846-
	9 10 10	₹ \ •• (10.55 20.55	*1693+03	.9431+03	-6.9
	700	457	1543	* T665+03	- P&G4+03	-107
) (C	077	1.01	. 7037+03	•9575+83	-7.2
	300	707	7707	* (PEG*+03	69347e03	e. T.
	* i		80	.7581+03	.9318+03	-7.5
	,,,,	160	9 8	17559+01	,9290+63	-7-1
	9 f 1 C	r e)	.7526+03	•9262+03	-7.9
1	700			10.88.67	.9234+03	1
	p (***	7.6	50+1/ 5/0	£0+5026.	N . 0 -
4		851		· 744463	-9177+63	
	310	178	3.6	.7416+03	.9150+63	9.6-
	523	156	8.6	.7389+63	•9122÷63	E 48-
	100	157	89 4	.7362+03	.9088+13	0.6-
	900	136	Bab	73,5403	•9254+03	-9.1
	012	111	8.6	NO+BUNK.	.9721+93	-9.3
	612		8.6	+7281±33	8988+63	4.6.
	00.7	109	9.00	•7255+03	10+036B	9-6-
	30.8	£84	B. 7	.7228+03	.8921+n3	6
	011	105	L 90	.72C1+G3	M L + 60 60 60 60	6.6-
	269	11.7	5.7	717E+F7	*C+VS&	1001-

(H3) (DEG C)				•		E-011		C-01-					200				11-		+03	+01	+03 -12+6				FOR THE PROPERTY OF THE PROPER			1.02				•	2001						-16.6						7	2012
(GRAM/M3)	. 8 790¢ U	.8763+03	4736+03	. 108	0+1898v	. 8654+03	.8627+03	.0603+03	. A 57.3+0.1	.8547+U3	. 6523+03	.8495+03	4669+0	*******	70 70 70 70 70 70 70 70 70 70 70 70 70 7	70 + F + F 0 + F + F + F + F + F + F + F	20444		. A295+03	6270	.8247+03	.8225+C3	•8203+03	. A180+0	.0158+03	704114	A 192+01	50+D704.	C-BACA.	.8022+03	7997+03	. 7971+£3	79854	1940261	20.040	PC+4446.	70+0146	1340F.	.7764.0	.7739+P3	.7712-	748A61	.7657+93	1630+03	.7634+73	.7577453
(MILLIBARS)	7122+03	.7096+03	1010101	.7044+03	1018103	.6992+03	1019969	.6941+03	315+03	.6890+03	.6864103	.6839+03	*6818403	6788+03	6763603	5D+85 / 0 ·		**************************************	44 10+01	MC+4-4-4	.6590+03	10059599	.6540+03	16516+03	.6492+03	TO THE TOTAL OF TH	10.0144	16395+03	.6171053	.6347+03	.6323403	•6299+63	.6276+03	.6252+33	CU162224	50-5029•			F1126117	MU+0804	.6066+03	- FD43+D3	.6025+63	5997+61	5975+03	.5952+03
(DEG C)	A - 3	8.8	N. B.	8.2	8.1	7.9	7.7	7.6	7.4	7.3	7.1	6.9	6.7	6.5	6.3	6.1	8 • 9	r- v		7 - V	3	5 4	H. A	0.4	3.7	7	7 0	7-6		2.5	2.5	1.8	1.1	1.5	Bet	2.3		•	9	- F-	9.		3	3		2
(DEG)	116	130	129	123	129	129	118	115	123	112	Opp	102	111	103	193	115	1117	101		971	110		133	122	130	14.5	0 11	971	n 4 n	110	0.3	173	131	133	15.1	149	151	153	791	U + •	4	0 3	755	: 0	156	175
(FIVSEC)	000	010	9	230	611	011	010	012	910	110	3	015	012	011	012	013	800	800	612	010	920	200	800	00.6	011	000	3 00	920	910	500	1 d	002	001	100	700	700	613	012	613	910	015	1 1	200	2 .	770) ~ C
, e r ,	1,000	01010		01010		010530	יושאנוני	016769		210011		20110	1200	011300	011400	11523	C1160G	011760	008110	011960	612000	001710	012700	12400	612500	C12603	012760	G12803	512963	07.20.00		0135.00	0045	613500	013600	613760	C13852	613900	C1433E	614100	114200	514305	20 950		01400	

TABLE 5. (Continued)

TABLE 5. (Continued)

(FT)	(FT/5EC)	(050)	(056 C)	(MILLIBARS)	(GRAH/H3)	
02000	110	28.6		104664	-6420+B3	e21.1
92010 ₀	011	296	5-14-	20+2404	10.0449.	-27.3
1,25,200	411	29.0	-11.7	4827:03	6428+03	-27.0
626369	410	302	-11.9	******	.6408+03	-27.6
625470	110	308	-12.1	. 4.789+C3	.6387+03	-27.1
520500	210	80 N	-12.2	E0+044+	* 6 366+0W	-27.9
920400	410	417	412.4	*#751+03	194941.44	-2101
020700	013	N C	-12.6	.4732+03	· 6 325 + 03	-28.2
020800		415	-12.6	- WII4+03	• 6 305 + 03	#ZBAB
020900	018	317	0 • n = 1	NO+869#*	NO+8829*	-28.5
021000	510	230	e13.2	.4676463	.6268+23	-28-7
521166	***	e de la companya de l	1984	•#658+D3	.6244+03	-28.6
021200	910	121	- Z of ta	10+619401	64225+03	-29 A D
021300	* 10	M (0.01	. 4620+03	.6206+03	-29.1
021400	010	325	B 1 4 c 1	***************************************	6186+03	-28-1
02120	010	322	M = 7 - 1	いの・オロのき。	•6167+03	1-62-
221600	110	925	9.44.6	-8565e03	-616A+03	-29.4
621700	\$£0	0 () () () () () () () () () (90 (1 3 (1)	グロートないか。	50+6219*	1.62.
-	200	7		4528203	- Sugartas	27272
004120	2.00	10 C	7 · 6 · 6 · 6 · 6 · 6 · 6 · 6 · 6 · 6 ·	70+110+1	50+1604 	
1440mm	710		2010	20.25.44	667.203	79072
	2 0		6 C V	70+0-4-4	70++60	
022400	210	44.	7 7 5	2040244	A 24 24 24 2	4.074
022400	n 4		7 1 9 4	7017644	70 - 40 d	
622500	016	34.2	-16.8		10+140A.	-31.2
6224.00	Dia	3.4.7	-17.1	A 185+03	5961+01	-3108
622703	015	336	-17.3	.4367+03	. 5945+03	-31.e
022800	01.7	33.0	-17.6	-4 X50+03	. 5927+03	-11-6
025200	015	340	-17.6	.4332+03	.5909+03	-32.0
271000	410	27.7		4315+03	.5491+63	-12.2
623100	016	50 C	M • 60 + 1	*4297+03	10.404.00	-32.4
023250	man man	222	91849	***************************************	13455453	avz.
023300	a (332		MO + MA MO + M	70+0700°	9.25.
223500	017	116	10.4	422404	1000 B	-11-1
G2360a	nta	110	2.919	- W210+03	. 5782+03	
G2370C	018	331	-19.8	E0+8014"	.5763+03	-13.5
523800	01.7	12.2	-20.0	176+03	-5785+0z	-33.7
2239ca	018	327	-22.03	.4159+03	.5727.03	-33.9
124650	014	329	-25.5	-6162+03	.5710+C3	-3401
224103	017	322	-20.7	.4125+03	.5691+13	-34.3
בשביים	020	121	-23.9	ALICARDI	45672+Ω3	4.42.
524309	619	31.7	1910	10-100s	.5653+03	9**6
-24450 	022	115	-21.3	*8074+03	5634+03	-Ibe7
.2450C	0.22	916	in t	NO+8503*	.0618+03	O
AC ABULE	530	210	70770	20 27 80 8 4	227776	126.2
0247E	2 4 2 2 2	9 47 10 14 10 14	\$ - 12 C		20+8/66°	7 - 67 - 1
0.0467						

DEW POINT	(0.66 C)	-35,7	-35.9	-36.0	-36.2	36.9	-36.5	-36.7	-36.9	-17.1	-37.2	-37.6	-37.6	-37.8	-37.9	-318+1	N. 9H.	- 18.5	-38.7	-18.8	-39.0	-10.2	-39.4	-19.6	-39.8	-40.0	2.04-	-#3c#	9.04-	-40.A	C • T +-	-41.2	***	-4146	8-17-	-42.0	7.5	-42.5	-42.7	42.9	1 - 6 3 - 1	-41.4	-43.5	-43.7	0 • 3 \$ 1	-44.2	3.331	9.44-	0 • 1 1	-4501	-45.3
DENSTIY	(GRAM/H3)	.5523+03	.5505+03	. 5487+93	.5470+03	.545Z+D3	.5434+33	.5417+03	.5399+03	5 182+03	.5365.03	.5347+03	.5329+03	.5111+63	.5293+03	5275403	.5257+03	.5239+03	.5221+93	5203+03	.5186+03	.5168+n3	.5151+03	.5134+03	.5117+03	.5100+03	.5084+03	.5067+03	.5050+03	.5€3&+D3	.5017+03	.5001+03	*#988+U3	*#969+F3	*4954+03	-4938+C3	.4923+03	.4907+03	•4892+D3	* 4876 • D3	.4661+73	. 4846+G3.	\$G+D£81°	.4815+03	BU+C087.	4785+53	8U+0140	4 755 ± 73	. 4740+03	4725+73	.4713+03
PPFSSUPF	(MILLIBARS)	1975+01	.3958+03	3942+C3	.3926+03	13909+03	.3893+03	1877+07	.3861+03	.3845+03	.3829+03	13,13,03	.3797+03	.1781+03	.3765+03	3750403	.3734+03	.3718+03	. 3703+63	1687+03	.3672+n3	.3657.03	.3641+03	.3626+03	.3611+03	. 359c+D3	•3580+03	*3565+D3	.3550+03	.15.15+0.1	.3520+03	3505+03	**************************************	10+9245	.3461+03	3446+03	.3431+03	.3417+03	.3402+D3	.3358+C3	.3373+03	3359+03	.3345+03	1313401	.3316+03	-3322+03	.3297+03	.3273+63	.3259+03	3245+63	.3231+03
TEMPERALURE	(DEG C)	-22.5	-22.7	-23.C	-23.2	-23.4	-23.6	-23.9	-24.1	-24.3	-24.6	-24.8	-25.0	-25.2	-25.4	*25.6	-25.7	*25.9	-26.1	26.3	-26.5	-26.7	-26.9	-27.2	-27.4	-27.6	-27.8	-28.1	-28.3		-28.8	-29.5	-29.3	-29.5	-29.8	-33-1	E 3C.	=13a6	Ø*(1)%	=31.02	-31.4		-32.C	-12.3	+ 42 a S	-32.0	-33.1	-33.4	-33.7	-33.9	-34.5
HIND DIRECTION	(DEG)	12 C	316	119	318	314	317	314	316	316	316	316	309	313	308	309	312	101	313	311	562	304	302	101	307	304	308	301	302	296	284	283	273	27.7	271	271	275	270	275	271	275	275	271	274	271	273	276	272	274	212	270
MIND SPEED		030	031	035	032	0.15	980	0.74	#£O	032	033	032	033	0.7.1	027	026	023	025	023	621	021	018	910	521	021	922	022	021	072	019	021	921	022	522	021	023	023	023	200		525	024	920	624	622	450	200	022	920	C22	023
At TITUDE	(FT)	025920	025160	025233	025307	.254ü2	C255C0	£25623	752700	C25800	625900	526039	026160	C262Cn	026300	626469	026550	526653	626765	626800	026900	527000	027150	027250	02730n	027400	527538	327669	027753	327800	ú2790C	228003	0291C7	.282JD	528300	628469	J28500	C2865C	. 28735	C2883C	328933	229205	C291C3	.29200	C29300		r295ca	٠.1	U29700	٠	L36625

	2711 2712 2713 2714 2715 2715 2715 2715 2715 2716 2717 2718 2718 2718 2718 2718 2718 2718
	27.3 21.6 21.5 21.5 21.5 21.5 21.5 21.5 21.5 21.5
	215 275 277 277 277 277 278 278 277 277 277 277
	215 217 217 217 2215 2215 2215 2215 2215
	217 219 219 219 219 219 217 217 219 283 289
}	275 275 275 274 277 277 277 277 277 289 289 289
	275 275 271 271 271 271 271 271 271 271 271 271
	219 2218 2218 2218 2218 2219 2219 2219 2
	2219 274 277 277 277 277 284 284 288
	274 275 275 277 277 277 283 284 288
	215 215 217 214 214 217 219 283 284 289
	275 277 277 277 277 283 284 289 289
	277 274 277 277 283 284 289 288
	274 277 279 288 289 289 288
	277 217 219 284 289 289
	279 284 289 289
	284 289 289 288
	284 289 288
	28.8
	28B
	288
	285
	289
	288
	292
	291
	29.1
	25.7
	29.6
	962
	Girl
	295
	29.7
	320
	297
	295
	29.5

LIIINDE	WIND SPEED	WIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	111111111111111111111111111111111111111
(FT)	(FT/SEC)	(DEG)	(DEG C)	(MILLIBARS)	(GRAM/M3)	(0 930)
635,000	0.74	294	-4.Z.3	.2574+03	*3969+03	day #-
035109	032	292	-47.5	.2562+03	.3955+03	6.64-
G35230	034	29 6	-47.1	.2550+03	3940+03	-50-1
C353C0	3 M CO	295	0.21-	.2538+03	.3925+N3	4-03-4
635463	072	29.5	-65.1	.2527+03	*3911+03	-5046
u355 23	0.15	293	148.3	.2515+03	.3896+93	-50.9
33562F	0.74	TOD	-48.5	.2503+D3	•3882+U3	-51.2
035760	032	304	148.7	.2492+03	.3867.03	4-15-
635850	CII	16.2	-48.9	-2461+03	1851+01	-51.7
035900	110	302	1-69-1	.2469+03	.3839+03	-51.9
.36000	633	299	- E - O - I	.2458+03	.1825+C3	-62.2
236100	0.35	296	5-64-	.2446+03	.3811+33	-52.4
03620	033	302	-49aB	. 24 35+03.	1197+03	-52,1
636300	032	298	-50°C	*2424+03	.3784+O3	-52.9
.J6ACC	0.15	299	-5 C - 3	2012401	17773+03	-53.2
036560	and C	208	5.05-	-2461+03	.3757+03	-51.4
C36600	010	103	-E9.7	2190+01	1744+03	46146
58730	042	301	7 9 9	270+01	1710+01	0.13-
	7 4 7 C	4 60 00	0 TO	00.0000 00.0000 00.0000	10 - D1 -	1.48
14.907	F	1.1	-61 6	2167471	270-103	4.43.
) f	1000	0.40	0000000	70 x 50 x 7 *	
047100	740	900	0 13-	27.75.07	76.77	9 9 9
		447	6 6 6 6	70.000	P (- 4 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	
22426	220	200	7075	22.827.79	20160021	19202
	80 F	867	4.00	.2313+03	.3651+13	
10.07 51	7 60	787	7.25-	2102+03	43658413	4555
03750	640	300	6.25-	.2292+03	.3625+03	-55.8
357600	048	299	-53.2	.2281.03	4.5612+g3	1-65-
037780	050	298	-53.4	.2270+03	13599+33	-56.3
627803	049	336	-53.7	*2259+G3	.3587+33	-56.6
3379 03	0.0	298	6 2 2 9	.2249+03	.3574+03	-56.3
33050	051	299	-54.2	22 18+03	1561+03	1-57-1
38100	051	301	F • 75-	.ZZZ8+03	.3545+93	-57.6
138200	651	101	-54.3	.2217+23	1530+03	E-Ba-
038300	053	305	1040	.2237+03	.3514+03	-58.5
038400	053	3,17	5 4 5 4	.2196+53	3499+03	-59an
0385 EB	056	305	- 15 to 5	.2186+03	.3483+03	1-55-
3386CF	0.6.2	127	=54.66	2176+03	▲ 3 868+03	-5949
3387C9	C62	9 F)	-54.07	.2165+03	3453+03	4.09-
36800	DAS	3	54.6	.2155+03	3439+03	-613-3
.369 _c 3	066	· (r)	10 37 10	.2145+03	. 34234.03	-61.3
39300	C68	- C3	0 435	2135+03	*34C7+03	-6148
G3912n	071	306	-88- -88-	.2125+03	3392+03	-61.9
239252	07.0	155	-55.	2115+01	*3377+03	-62.2
2393CF	073	303	-55+1	.2105+03	3362+03	-62.1
.39400	C34	346	-55.2	-2395+63	ECI+BANT.	
139513	076	ri Bi	-55.2	+2GF5+C3	.3333+03	-62.2
C396EC	27.0	151	-555-3	•2075+C3	.3318+03	-62.3
	676	# CP	+°55-	.2065+63	.3333+03	-62.4
C.158C.	575	325	-5545	+255503	3289+03	-5225
		3.2	11	FU TUTE	10701	* * * *

Color Colo	ALTITUDE	BIMD SPEED	MIND DIRECTION	TEMPERATURE	PRESSURE	DENSITY	UEN PULBI
1,	(FT)	(FT/SEC)	(05.6)		(MILLIBARS)	(GRAM/H3)	(DEG C)
10		075	306	855.6	.2036+03	.3260+03	-62.7
10	021043	076	306	-55.8	.2026+03	.3247+03	-62.7
The control of the	CAG2CO	076	306	-56.0	.2016+03	3234+03	-62.7
10	040303	077	304	-56.2	.2007+03	.3222+G3	-62.7
077 104 -56.5 1976+013 1310+013 076 105 196.001 1312-13 076 105 196.001 1312-13 071 105 196.001 1312-13 071 105 196.001 1312-13 071 107 107 1312-13 071 107 107 1312-13 071 107 107 1312-13 071 107 107 1312-13 071 108 186.10 1312-13 072 109 186.2 186.2 073 109 186.2 186.2 074 108 186.2 186.2 077 109 186.2 186.2 077 109 186.2 186.2 077 109 186.2 186.2 077 109 186.2 186.2 077 109 186.2 186.2 077 109 186.2 </td <td>CAOACO</td> <td>077</td> <td>304</td> <td></td> <td>-1997+G3</td> <td>.3239+03</td> <td>-62.7</td>	CAOACO	077	304		-1997+G3	.3239+03	-62.7
10 10 10 10 10 10 10 10	208042	7.10	30 P	-56.5	.1986+03	.3197-03	-62.7
10	242652	C78	101	5667	1976+03	-3184+C3	-62e7
10	646763	910	35.00	5.95-	*1969+G3	.3172+03	-62.7
10	245,600	070	395	=57.4	•1959+03	3160+03	-62.1
11	242969	840	306	-57.3	.1950+03	50+V+IN*	-62.7
OTT ST	341969	971	366	=57.5	1941+01	.3135+03	-62.7
Color	C#1100	073	100	-57.7	.1931+07	.3123+43	• 6666-
071 107 -56.1 191100 1009***********************************	041250	071	101	-57.9	1922+63	.3111+03	-6666-
070 308 -56.5 1904-01 -508.00 1004-01<	041300	110	701	-58.1	.1913+63	.3099+03	-6666-
070 338 -58.5 -1885.03 -3075.03 071 308 -58.5 -1865.01 -3075.03 072 303 -58.7 -1865.01 -305.03 072 301 -58.9 -1865.01 -305.03 072 302 -59.5 -1865.01 -3077.03 071 302 -59.6 -1840.02 -3016.03 071 302 -59.6 -1840.02 -3017.03 072 303 -59.6 -1840.03 -2918.03 073 304 -60.4 -1840.03 -2918.03 074 304 -60.4 -1762.03 -2917.03 074 304 -60.4 -1762.03 -2917.03 074 304 -60.4 -1762.03 -2917.03 074 304 -60.4 -1762.03 -2817.03 074 304 -60.4 -1762.03 -2817.03 075 306 -60.4 -1762.03 -2817.03 <t< td=""><td>04140</td><td>010</td><td>368</td><td>-59-3</td><td>1954+03</td><td>.3087+03</td><td>*6665=</td></t<>	04140	010	368	-59-3	1954+03	.3087+03	*6665=
671 395 -58.7 -1865801 -5103.01 072 303 -58.7 -1865803 -30510.03 072 303 -58.1 -1865803 -30510.03 072 303 -59.6 -184503 -30510.03 070 301 -59.6 -184503 -301403 071 302 -59.6 -184503 -291403 071 303 -59.6 -184503 -291403 072 303 -59.6 -184603 -291403 073 303 -60.3 -184603 -291403 074 303 -60.3 -182603 -291403 075 304 -60.4 -173603 -291403 074 304 -60.4 -173603 -291403 074 304 -60.4 -173603 -291403 074 304 -60.4 -173603 -291403 074 304 -60.4 -173603 -291403 074	041550	070	338	ភា ១៦១	.1895+03	.3675+03	-6666-
072 103 -56.9 -1862603 -305103 072 301 -56.9 -1862603 -3155103 072 301 -59.5 -1868603 -302703 072 301 -59.6 -1868603 -302703 071 301 -59.6 -1868603 -302703 072 302 -59.6 -1868603 -2786613 071 303 -59.6 -1868603 -2786613 072 303 -60.3 -1805603 -2786613 073 304 -60.4 -1805603 -2786613 074 304 -60.4 -176603 -2986613 073 304 -60.5 -176603 -2986613 074 304 -60.6 -176603 -2986613 075 304 -60.6 -176603 -2986603 074 304 -60.6 -176603 -2986603 075 310 -60.6 -176603 -2986603	341669	671	305	-58.7	-1865+03	.3063.03	-0666
077 711 -58.1 11842403 -31034033 072 302 -59.6 -1849403 -3104403 070 301 -59.6 -1849403 -3104403 071 303 -59.6 -1849403 -2914403 071 303 -59.9 -1843403 -2914403 072 303 -59.9 -1843403 -2914403 074 303 -60.4 -1843403 -2914403 072 303 -60.4 -176403 -294403 073 304 -60.4 -176403 -294403 074 304 -61.4 -176403 -294403 074 304 -61.2 -176403 -294403 074 304 -61.2 -176403 -291413 074 316 -61.2 -176403 -286403 075 316 -61.2 -176403 -286403 074 316 -61.2 -176403 -286403 <t< td=""><td>C4173C</td><td>072</td><td>303</td><td>-58.9</td><td>.1876+03</td><td>.3051+03</td><td>-6666-</td></t<>	C4173C	072	303	-58.9	.1876+03	.3051+03	-6666-
172 302 -59.5 -1848-613 -3027-03 -59.6 -1848-613 -30127-03 -59.6 -1848-613 -3013-03 -59.6 -1848-613 -3013-03 -59.6 -1848-613 -3013-03 -59.6 -1848-613 -2914-61	CA18CO	329	101	-59+1	.1867+03	1019+03	-6666-
072 331 -59-5 1889203 3018403 071 301 -59-6 1840-03 3018403 071 302 -59-6 1840-03 2918403 072 303 -59-6 1840-03 2948403 073 303 -60-3 1840-03 2948403 074 304 -60-3 1840-03 2948403 075 304 -60-3 1840-03 2948403 074 304 -60-4 1740-03 2948403 075 304 -60-6 1740-03 2948403 074 304 -60-6 1740-03 2948403 075 304 -60-6 1770-03 2948403 074 304 -60-6 1770-03 2948403 075 304 -61-1 1770-03 2948403 074 304 -61-1 1764-03 2948403 075 304 -61-1 1764-03 2948403 074	0961#2	672	302	59	.1858+03	.3027+03	-6666-
070 301 -59.6 .1840-03 .3913-03 071 302 -59.6 .1822-03 .2978-03 072 303 -59.6 .1823-03 .2978-03 071 302 -60.3 .1863-03 .2978-03 072 303 -60.3 .1784-03 .2946-03 072 304 -60.4 .1784-03 .2946-03 072 309 -60.5 .1784-03 .2948-03 073 304 -61.6 .1770-03 .2948-03 074 304 -61.1 .1754-03 .2948-03 074 304 -61.2 .1762-03 .2948-03 074 304 -61.2 .1762-03 .2948-03 075 304 -61.2 .1764-03 .2948-03 074 304 -61.2 .1764-03 .2948-03 075 308 -61.2 .1764-03 .2948-03 075 316 -61.2 .1764-03 .2948-03	042303	072	331	-59.5	.1849+03	.3016+03	-6666-
071 302 -59.4 1823-03 2291-03 0A7 303 -65.4 1823-03 2294-03 0A7 303 -65.4 1865-03 2294-03 0A7 229 -60.4 1794-03 2294-03 0A2 304 -60.4 1794-03 2294-03 0A2 304 -60.4 1794-03 2294-03 0A7 304 -60.4 1762-03 2294-03 0A7 304 -60.4 1762-03 2294-03 0A7 304 -61.2 1770-03 2294-03 0A7 304 -61.2 1752-03 2294-03 0A7 310 -61.2 1754-03 2284-03 0A7 310 -61.2 1754-03 2284-03 0A8	042100	070	301	-59.6	.1840+03	.3903+03	-6666-
OTC SUB	28.22.0	073	362	-59.6	.1832+03	.2991+03	-9999
D69 302	342330	070	303	-59.9	.1823+03	.2978+93	-6666-
Decision Color C	042400	690	302	-65.1	.1819+03	.2966+13	-6866-
0.69 3GB -60-6 -1764603 -2244103 0.72 3Q4 -60-6 -176403 -2929++3 0.72 3Q4 -60-6 -1760-0 -2917-03 0.72 3Q4 -60-6 -1760-0 -2917-03 0.74 3Q4 -61-1 -1762-0 -2803+03 0.74 3Q4 -61-1 -1762-0 -2803+03 0.74 3Q4 -61-2 -1762-0 -2868-03 0.74 3Q4 -61-3 -1762-03 -2868-03 0.75 3Q6 -61-3 -1764-03 -2868-03 0.75 3Q6 -61-6 -1714-03 -2868-03 0.75 3Q6 -61-6 -1714-03 -2868-03 0.71 314 -61-6 -1714-03 -2818-03 0.64 314 -61-6 -1714-03 -2818-03 0.64 314 -62-6 -1624-03 -2734-03 0.65 312 -62-6 -1624-03 -2710-03	042500	071	295	-60.3	.1805+03	.2954+03	-6666-
072 299 -6C.5 -1736-03 -2929+-3 073 304 -60.6 -1770-03 -2929+-3 072 304 -61.6 -1770-03 -2915-03 074 304 -61.6 -1752-03 -2893-03 074 304 -61.2 -1752-03 -2863-03 075 304 -61.2 -1755-03 -2863-03 075 306 -61.2 -1756-03 -2863-03 075 306 -61.2 -1756-03 -2863-03 077 310 -61.5 -1756-03 -2863-03 078 310 -61.5 -1756-03 -2863-03 079 310 -61.5 -1756-03 -2863-03 071 314 -61.5 -1758-03 -2863-03 064 314 -61.5 -1758-03 -2866-03 055 312 -62.5 -1660-03 -2757-03 064 312 -62.5 -1660-03 -2757-03	042600	690	308	-60.4	.1796+03	.2941+03	₹6866-
073 301 -60.6 -1779sp -2917a3 072 304 -60.6 -1770sp -2917a3 073 304 -61.1 -17540g -2803sp 074 304 -61.2 -17540g -28040n 073 306 -61.3 -174540g -28040n 073 306 -61.3 -174540g -28040n 073 306 -61.3 -174540g -28040n 073 316 -61.5 -174540g -2804sh 074 316 -61.5 -171840g -2845sh 075 316 -61.5 -171840g -2845sh 076 314 -61.5 -171840g -2845sh 076 314 -61.5 -171840g -2765sh 086 314 -62.5 -1640sh -2755sh 086 312 -62.5 -1640sh -2755sh 086 312 -62.5 -1645sh -2751sh 088 </td <td>C\$ 2759</td> <td>072</td> <td>299</td> <td>-60.5</td> <td>.1788+03</td> <td>.2929+~3</td> <td>-6666-</td>	C\$ 2759	072	299	-60.5	.1788+03	.2929+~3	-6666-
072 304 -65.6 .1770+0 .2805+73 074 334 -61.1 .1754-03 .2864-03 074 334 -61.2 .1754-03 .2864-03 073 336 -61.3 .1754-03 .2865-73 075 308 -61.3 .1754-03 .2855-73 075 310 -61.6 .1716-03 .2855-73 077 314 -61.6 .1716-03 .2855-73 078 314 -61.6 .1716-03 .2853-73 079 314 -61.6 .1716-03 .2813-03 064 314 -61.6 .1716-03 .2731-03 064 314 -62.6 .1664-03 .2731-03 064 315 -62.6 .1669-03 .2716-03 064 315 -62.6 .1669-03 .2716-03 064 315 -62.6 .1664-03 .2716-03 066 314 -62.6 .1669-03 .2716-03 <	342833	673	361	-60-2	1779+03	-2917+53	6666
312 313 -61-5 -1762403 -28934C3 074 334 -61-1 -1745403 -2880403 073 336 -61-3 -1745403 -2865403 075 306 -61-3 -1745403 -2865403 075 309 -61-6 -1722403 -2855-03 075 310 -61-5 -1719403 -2855-03 076 316 -61-5 -1719403 -2855-03 077 310 -61-5 -1719403 -2831-03 078 314 -61-5 -1719403 -2831-03 064 314 -61-5 -1719403 -2731-03 064 314 -62-5 -16-64-03 -2731-03 065 312 -62-5 -16-64-03 -2793-03 066 312 -62-5 -16-64-03 -2793-03 066 312 -62-5 -16-64-03 -2795-03 066 312 -62-5 -16-64-03 -2795-03	C#290F	575	304	-63.8	.1770+g3	•2905+⊓3	-6666-
074 334 -61.1 1753.03 -2860-03 073 356 -61.2 1745.03 -2864.013 075 306 -61.5 1734.03 -2855.93 075 310 -61.6 1724.03 -2855.93 077 310 -61.6 1719.03 -2853.43 078 314 -61.6 1719.03 -2853.43 064 314 -61.6 1714.03 -2833.43 064 314 -62.0 1504.03 -2734.03 064 314 -62.0 -1624.03 -2759.03 065 315 -62.0 -1664.03 -2759.03 066 315 -62.0 -1669.03 -2759.03 066 315 -62.0 -1669.03 -2759.03 066 315 -62.0 -1669.03 -2759.03 066 312 -62.0 -1669.03 -2751.03 068 313 -62.0 -1659.03 -2751.03	243020	272	303	26165	1762+03	.2893+53	-9999
074 326 -61.2 -1745403 -2868403 073 330 -61.4 -1736403 -2855473 075 309 -61.6 -1736403 -2855473 073 310 -61.6 -1718403 -2853473 074 310 -61.6 -1718403 -2833403 075 314 -61.6 -1718403 -2813403 064 314 -61.6 -1718403 -2793403 064 314 -62.6 -1674403 -2793403 066 315 -62.2 -1664403 -2793403 066 312 -62.5 -1664403 -2793403 066 312 -62.5 -165403 -2734503 066 312 -62.5 -1653403 -2734603 066 313 -62.6 -1653403 -2734003 066 313 -62.6 -1653403 -2734003 068 314 -62.6 -1653403 -2559603 <	043100	940	304	-61.1	.1753+03	.2580+03	-6666-
073 336 -61.3 -1736+03 -2855+73 075 309 -61.6 -172401 -2855+73 073 310 -61.6 -171403 -2855+73 073 310 -61.6 -171403 -2813403 074 314 -61.6 -171403 -2813403 058 314 -61.6 -171403 -2813403 064 314 -61.6 -171403 -281403 055 314 -62.6 -164403 -273403 056 315 -62.2 -1669+03 -273403 056 312 -62.5 -1669+03 -273403 056 312 -62.5 -1669+03 -273403 056 313 -62.5 -1659+03 -273103 068 313 -62.5 -1659+03 -273103 068 313 -62.6 -1629+03 -273103 068 313 -62.6 -1629+03 -273103 <th< td=""><td>GN 3200</td><td>#Z0</td><td>136</td><td>-51.2</td><td>1745+03</td><td>.286A+U3</td><td>-6666-</td></th<>	GN 3200	#Z0	136	-51.2	1745+03	.286A+U3	-6666-
075 309 -61.6 -17.28+D3 -2843+C3 077 310 -61.6 -1719+O3 -2833+C3 072 310 -61.6 -1713+O3 -2813+C3 071 314 -61.6 -1712+O3 -2813+C3 068 314 -62.6 -1694+O3 -2793+C3 066 314 -52.0 -1694+O3 -2793+C3 066 314 -52.0 -1694+O3 -2793+C3 066 315 -62.2 -1669+O3 -2793+O3 066 312 -62.2 -1669+O3 -2757+O3 066 312 -62.2 -1669+O3 -2757+O3 066 312 -62.6 -1643+O3 -2757+O3 066 312 -62.6 -1643+O3 -2751+O3 068 312 -62.6 -1629+O3 -2751+O3 068 312 -62.6 -1629+O3 -2696+O3 068 314 -62.6 -1629+O3 -2696+O3	C+3300	073	308	-61.3	.1736+03	.2855+73	-6666-
073 310 -61.5 .1719+03 .2833+03 072 379 -61.5 .1713-03 .28134-03 071 314 -61.5 .1713-03 .2813-03 064 314 -61.5 .1540-03 .2721-03 065 314 -62.5 .1660-03 .2769-33 066 315 -62.2 .1669-03 .2757-03 165 312 -62.2 .1669-03 .2757-03 166 312 -62.5 .1664-03 .2757-03 166 312 -62.5 .1644-03 .2757-03 166 312 -62.5 .1644-03 .2757-03 166 312 -62.6 .1644-03 .2757-03 166 312 -62.6 .1643-03 .2751-03 168 312 -62.6 .1629-03 .2751-03 168 314 -62.6 .1629-03 .2666-03 169 314 -62.6 .1629-03 .2751-03	CASADO	075	109	-61.4	-172a+D3	.284X+CI	-9899
072 379 -61.0 -17.11.003 -28139.23 071 314 -61.0 -17.2403 -28040.23 064 314 -52.0 -16.64.03 -27031.03 064 314 -52.0 -16.64.03 -27031.03 065 312 -62.2 -16.74.03 -2769.03 065 315 -62.2 -16.74.03 -2757.03 165 312 -62.2 -16.14.03 -2757.03 166 312 -62.5 -16.14.03 -2795.03 166 312 -62.5 -16.14.03 -2795.03 168 313 -62.6 -16.34.03 -2795.03 168 313 -62.6 -16.34.03 -26.66.03 168 314 -62.6 -16.24.03 -26.66.03 168 314 -62.6 -16.24.03 -27.214.03 168 314 -62.6 -16.24.03 -27.214.03 168 314 -62.6 -16.24.03 -27	C+3867	073	310	-61.5	•1719+03	.2633+03	-6666-
G71 314 -61.00 -61.00 -51.04	CA 3655	072	129	-5107	-1711+02	.2813+C3	-6666-
068 315 -51°5 -1624¢03 -2793¢03 064 314 -52°C -166403 -2781¢03 065 312 -52°C -1669¢03 -2781¢03 066 312 -62°C -1669¢03 -2785¢03 066 312 -62°C -1661¢03 -2785¢03 066 312 -62°C -1653¢03 -2733¢03 068 313 -62°C -1629¢03 -2731¢03 068 312 -62°C -1629¢03 -2751¢03 068 312 -62°C -1629¢03 -2751¢03 068 312 -62°C -1629¢03 -2666¢03 068 314 -62°C -1621¢03 -2666¢03	£437.00	170	314	3•19-	•17 ₂ 2+83	.2836+C3	• 66661
G64 314 -52.0 -1666+03 -2731+03 065 312 -62.2 -1678+03 -2751+03 066 315 -62.2 -1661+03 -2755+03 066 312 -62.5 -1653+03 -2745+73 066 312 -62.5 -1653+03 -2743+73 066 313 -62.6 -1645+03 -2713+73 068 312 -62.6 -1627+03 -2713+3 068 312 -62.6 -1627+03 -2713+3 068 314 -62.9 -1621+03 -2666+03 1068 314 -62.9 -1621+03 -2666+03 1069 314 -62.9 -1621+03 -2674+03	CA 38C0	068	715.	-5105	-1694-03	.2793+23	-6666-
12	こもろうじつ	490	314	-52°C	•1686+O3	.2731+03	-9999-
1066 315 -62-2 -1669-03 -2757-03	C44050	365	312		.1678+DI	.2769.33	-3666-
12	044100	990	318	-62.2	.1669+03	.2757+93	-6666-
C67 312 -62.5 -165303 -2733+7.5 106 715 -62.6 -1645403 -2721:03 113 -62.7 -1627+03 -2711:03 112 -62.6 -62.6 -1621:03 114 -62.9 -1621:03 -2666+03 11621:03 -63.1 -1613:03 -2674:03	44200	290	21.2	-6203	1661+03	.2795+C3	-6666-
G66 113	008440	193	312	162.5	.1653+03	.2733+53	• 6666-
G66 113		0,00	115	-62.6	. 1£45±03	.2721+93	46665−
2	175887	990	113	1-25-1	.1637+03	.2713+33	* 5666-
44755 068 314 -62.9 .1621+03 .2666+63 .48833 .2613+03 .2614+63			31.2	-62aE	1629+62	,2696+C3.	3884
84827 064 111 -6551 11513427 AZB/14473	20/440	890	# C P P	-62.9	.1621+03	.2666+03	6466 -
		064	111	-6.54	1613+27	*2674+F3	-6666-

(FT) Cason	(FT/SEC)	(0) (0)			(27/7700)	10 3901
CASALA			י מנים	INTELIBARON		
	062	150	263.3	1557+03	.2651+53	-6666-
C#51C7	290	306	4-63-4	.1589+03	.2640+03	-6666-
08 5203	063	33.8	-63.66	1581+63	2628+03	-9999
0453.00	P)	310	-63.7	.1574+03	.2617+03	-6666-
245400	595	10.0	-63.8	.1566+63	.2636+93	* 6666-
045500	290	311	-63.9	.1558+03	.2595+03	-6666-
5.454.2	562	312	1 49	1553+63	.2583+M3	-6666-
045700	557	315	-64.2	.1543+03	.2572+03	-9999
Tag Bull	152	31.7	-6403	.1535+63	2561+03	-6666-
145917	05.5	315	-64.5	.1528+03	.2550+63	-6666-
UB6000	050	316	-6446	.1523103	.2539+03	-6666-
546130	545	616	9.791	.1512+03	.2529+63	-6666-
246230	09.2	312	0.00	1505+03	2518+B3	-9999
385150	041	712	-65-1	10+2641	.2508+03	*6666-
Cara Co	0.12	312	1.54=	140300	7408461	0000-
2000	0.78	112	7 7 7	70+7044	2887+01	-0000
) C	4 1	6 6 6	P (4 UP 3 V	*******	0000
	777	414	1.00	2010111	24674-1	-0000
	200	,	A C 1	MC+144+	2042401	0000
0440:0	3 2 0	tak.	-44-2	4 1 1 4 4 () 4	-2447+03	-0000-
	346	101	7.99=	10 CO 10	76+7+6	0000
1671.7	0.14	208	-66-7	140403	.2428+U3	-0000-
2074) (C	200	0 4	10+24+1	2418+53	6660-
707/407	015	200	-47.2	1425+03	2409+53	-6666-
7007	1000	29.5	7 2 4	14170	2400+03	6666-
24750	215	201	-47.7	20404.4	2701+111	-0000-
25475	200	286	1.69		2782+03	0000-
477-0	04.1	22.8	£ 83.5	1396+03	.2373+63	-9866-
20067	. a0	286	-68.5	1389+03	*2164+D3	-9999
F 79.7	190	286	-68-7	1392+03	.2355+13	-6666-
CARGOD	543	28.2	269.0	11175+61	.2347+E3	-6666-
046100	243	285	-59.1	.1366+03	.2336+93	-6666-
G48235	000	279	-69-3	1361467	2125+03	*6666-
C48353	9#6	27.7	1.69-	.1354+63	.2316+C3	*6666*
0.464.3	25.2	234	46946	1348+53	2305+03	-8688-
249500	050	272	-69-6	.1341+03	.2296+53	-6666-
246602	05.3	271	6 69	1334+53	.2286+D3	-3999*
J#671.7	E 400	274	-73.5	11277+03	.2276+03	-3999
- Chap		275		11255+63	2266+23	*8666*
140007	14 67	276	-7.3.3	MC+3MM	.2257+03	-3999
-49CC3	05.1	279	-72.5	13:7+03	.2247+53	6566-
7,1910	350	287	-12.5	.1300+03	.2235+r3	-6666-
457.7	283	264	-7:-	1294+53	.2223+13	₹6666-
001697	ر ، ر ،	295	4-12-4	.1297+03	.2212+03	6060-
- 1.94m	546	296	-7.0.4	*12E1+ū3	2200+63	-3666-
"J864"	242	363	+ L-	.1274+53	.2169+03	*6666
3456.C	C41	302		-1265453	.2177±03	•6656-
276840	C.7.S	313	-7C.3	.1261+03	.2166+ 13	-6666-
435.2	0.1	118	7-3	1255+07	A2154+73	-9996

2	(FT/SEC)	(DEG)	340:401	THE STATE	DENSITY	DEN POTN
\$:	627	345	-25.2	(FILLIBARS)	(GRAH/H3)	(DEG C)
20170	0.52	34.1	-70-2	173.501	2112+03	-9999
	910	132	-73.3	1220403	.2121+03	6666-
10 C C C C C C C C C C C C C C C C C C C	010	# # M	-75-3	1221.01	2000	-9999
) u	623	332	-75.4	1017171	5Ú+T017•	6666-
100000	6.0	336	1-10-4	121144	2000	
(5,7:7	0.00	317	-75-4		20.40.20	6666-
	*10	313	77.5		26.72.72	-9999
30800	611	319	2.14	50+6577•	• 2060+03	6666-
3000		288	-70.4	11 22 03	2050+03	-9999
		29.7	9	50+9811•	.2540+93	6666-
221122	616	a Cr		•11E3+G3	-2330+33	6666-
3512cn	025	291		-1174+63	.2727+33	-6666-
621155	028	292	74.	1168+03	.2010+03	-6665-
2516CC	032	288		.1162+03	.2001+63	6666-
008180	86.73	106	Renta	1156+03	1991+03	0000-
-516 EA	~		6-10-0	.1150+03	.1982+03	0000
051750	400	***	-71si	1145+63	1972-01	0000
151823	167	962	-71.0	.1139+63	.1963+03	6000
C519C0	023	749	-71.1	11133+03	PC 42 50 F (6666
JE 2006	9 6	182	-71.1	.1127+03	1040+7	2222
3521.0		718	-71.2	1121+03		4666
1522.0		267	-71.2	1116+03	102401	7777
(523CP	770	28.7	-71.2	1110.03	00 + 10 m	6666-
5.20.00	200	262	-71.1	-1104+03	10000	-9009-
157577		285	-71-1	109945	10 + 10 a r	6666-
	2	282	-71-1	10-1001	200.200	-9999
200.20	6.1	28.5	-71.1	10 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	**************************************	6666-
	323	268	-71.1	100001	41875463	-6666-
•	626	27.7		5047616	50+5000°	-6606-
3 6 4	CZB	25.3	-71.3	107101	1855+73	-3888
	3.2	27.7	-11-	50.4.0	51+0+0T•	-6666-
	523	285	-76	1966-61	1836+73	-9999
	635	295	6-04-	50,000	• 1826+73	•6666-
7777	035	293	-7:-7	10.00	1816+03	₹6666-
	920	299	-70-6	7044401	*1909+03	-6666-
33300	0.12	301	-73.5	10101	41795433	-9999
9	0.42	36.1	2 - 6	73 2 7 7 7 7 7	.1785+13	•6666-
2000	C31	297	7. 1	20.200	1775-53	-6666-
	624	3.14		• 102013	.1766+03	-6666-
	200	377	7		1756+33	-9965
vi i	374	101	4 (. •) ← • (MO+0171.	.1745+73	-6665-
C2417	DMM.		7007	1612+63	1736.52	-9999
545	223	- W	D. C. G.	.1057+33	.1727-23	-6666-
しょうせい	(C)	0	3029	1302001	*1717+C3	6666-
		· (1.69-	.9972+32	.1707+53	-3005-
24527	7.6		65.6-	-9921+62	1698+71	0000
\$		5 7 1	-69-5	.9671+22	1689+63	2000
3	ecc		+•69=	.9821.02	A1679+C3	0000
4	3 w	200	-56.3	.9771+62	.1677+73	-0000
() (+ + 1)	45.		-£3 e3.	1241120		• • • • • • • • • • • • • • • • • • • •

TABLE 5. (Continued)

(3 930)		*6666-		41111	* 00 00 00 00 00 00 00 00 00 00 00 00 00	2777	90000	-22117	*****	27777	*****	4666-	*6666-	*8885	* A A A A A A A A A A A A A A A A A A A	****	• 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0000	* 65 66 1	4777	*****	0000	00001	0000=	-9993	*6666-	*6666*	* 0666T	* 6566 -	66666	-2277	• • • • • • • • • • • • • • • • • • • •	0666-	-9999-	-6666-	-9999€	-6666-	-9853	• 6666-	-6666-	**************************************	-0000	**************************************	00000	0000-	*6666+	*6666-	6000
() M / M V G G G	104C477	10.01	50055070	14.26**	.1618+05	c toniar .	1002413	1598-03	.1586+03	1578+73	.1573+93	41563463	·1482+£3	1196+03	.1328+03	1260463	.1189+03	11177111	.1065+73	1	9714+32	2015618	70+2998*	7-17070	7443+02	-7117+C2	6775+02	.6422+92	-6113+02	.5824+02	-55553+52	2548125	271100	C1+3854	4110+02	4108+62	.3921+32	3723±E2	.3533+02	3368+22	•3252+52 •3252+52	374947	.23.647	7 + C + C + C + C + C + C + C + C + C +	17.49.14.C	2.192+22	2273+52	
1 20 4 21 4 1 1 1	(MILLIERRS)	704748	20.46.40	29526412	20+924	204-246	.9362+02	9335002	.9266+02	.9241+52	.9194+32	.9148+D2	.8696+02	.8259+02	.7865+02	7482+02	.7119+02	-6776+02	.6452+02	6163232	20+6+85	.5569+32	.53(5+02	79.15.05		4-71-02	**************************************	.3970+52	- 3784+62	.3607+02	3439+02	3279402	2002-03	75.7367.	2711403	.2528+D2	2472462	2357+C2	.2249+62	.2147+62	*20502*	-1956+27	CL+0404.		70.00 / 7.	1586402	20,075T	
TENT CRAILURE	(DEG C)	7 6	3 • 6 • 6	2.89-	-69-1	-654-	-69.1	-69-1	-69-1	-69.2	7.69-	2.69.2	-58.6	3-44-	-66.6	-66.3	-64.5	=62.1	-62.2	-63.5	-63.4	-6102	(0) (0) (1)	-60ac	# 10 9 II	2.03-	3.46	-57.8	-57.4	4-27-4	-57.4	156.55 10.55 10.55	4000	# · · · · · · · · · · · · · · · · · · ·	7000	1	53.7		L • 15 •	4 4 5 4	4 • 7 % •	4 68	1 • £ 9 • 1	200	J)	
TWO CINECIDA	(056)	28.2	592	269	281	280	245	282	274	266	260	264.	268	25.5	247	277	313	123	525	224	251	283	361	128	9 T C	240	8 0 0	40L	127	801	121	3 وي	CB9	2 60		100	1 - 1) a) n		26.2	190	aı	C4 10		Cob	£4.5	37 H	4.1
MIND SPEED	(FT/SEC)	517	017	013	700	820	613	515	910	DIB	022	810	017	016	C15	014	012	920	3 LO	800	010	013	8,0	7.30	មា (ប	Zea	歌 f た U U U	- a) F	517	£ 2 4	220	()	632	533	13 CS	200	יי טע		0 M	026	233	820	-C3#	540	C33	0 P	347
LTITUDE	(FT)	25033	C251C2	522	5535	255430	5555	5.56	655760		•	56.70	657000		559000	0.000	C9079	16.2503		3	5005	6426.0	167000	LABECC.	58300	1002	271060	27.23.00	1460.00	.75-:-		177055		C79000	185535) () () (7700	. 8.5	C. L. 7.9	32475	101167	ij	3	24012

ALTITUDE	LIND SPEED	WIND DIRECTION	TEMPERATURE	PPESSUBE	DENCITY	
(FT)	(FT/SEC)	•	1056 13	(ATABE)	(C C A M 2 1)	1066.
22098	210	Dag		111102	2057452	
C07000	27.0	200	-4-7	127163	104440	0000
			7 - P	20.5.21.	7: + 10 6 4	• • • • • • • • • • • • • • • • • • • •
2000				7749177	791416	-
70044		675	9	2D+2911•	74.594.70	6666-
	1.1	790		11111.02	1696+32	-66660-
000101	120	293	M • # #	1062+02	1616+52	•6666-
15.25.30	027	268		1015+52	1545+02	-9999-
133063	035	710	N • 77-	.9727+01	•1478+CZ	-6666-
154050	0.18		7.77			*6666-
J22501	637	263	1-22-	.8872-01	-1349+02	-9999
106000	028	091	-42.9		.1284-02	-6666-
177543	C21	710	-41.0	.8114+01	.1222+CZ	-6666-
156350	021	USA	TALLS.	.7761+01	-1166+62	6666-
109933	027	089	8-0-4-	7425+01	-1113+92	-0000-
110000	1.1	049	() () a		10 11010 10 10 10 10 10 10 10 10 10 10 10 10 10 1	0000
111060		262	-30.6	. 4.708 ± 0.1	400000000000000000000000000000000000000	- 0000
112000	7 4 0	0 6	0 0	10 0 0 E 4 4	20.41010	0.000
10.00			3000	7745:164	20104	66664
11410) C	***	7 • F • • • • • • • • • • • • • • • • •	10.070.	11+46740	*****
115900	440	126	4 42		10000	00000
)) H	7 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	17.77.70	711.06.00	• 6666
7000	220		23263	1900000	10.010	-6666
	B (7.1	0 * * * *	43+6070*	10+2+9/*	• 6666
0.000	52.5	747	-5350	10.11111	*12934C1	6666
19000	2 PC	D-14	9754		10+6464	* 6666-
0.010	3.5	4 4 6	7.00	Themps	734844	-4444
000171	613	•	2017	10+11++	19+1959	6666-
.0.00	200			175057	17.7904	48686
	9 0		40.00	10820	10.7700.	*****
	- C	• 10	7045		775775	-1777
1260.0	9 C	0 M	P (17,7170	1.1.400.00	*****
1340.0			7416	- Paragraph	יייים ביבי	=7777
10000	7 2 6		n () () () () ()	13+7255	70+636#+	• 6666
		997	9017	12/10/2		46665
273621	C1 3	2.5	7.62	.3143+01	10+/9#**	• 6666-
		963	-5007	13421	12.717.00	-9999
020121		112	5-22-	10+9167	.4171+01	-6666-
37277	513	150	-27.5	•25£i:+11	* 4053+C1	-6666-
133557	910	166	-26.7	.2787-51	10+6555	-6666-
	216-	167	-27.5	27,5501	3845+71	*6666-
115/11	m (L)	P1 (0 P1	7-52-	4	3761+-1	•6600-
136255	£15	230		.2577	*3627.* Ti	-2099.
237756	016	236	-22.2	.2511- 1	.360501	• 6666 -
1,187,	17.7	241	-25.4	. +34454	10+6645=	-6606-
13651	S:0	E SC	-3- · 6	.2303+01	.3423+71	• 6556-
		229			37.42.42.	-9933
372745	26.73	SI PEI	-27.ê	.2262+01	3212+41	*666¢-
1925.0		- 246		21£E+51	. 3234+F1	-3633
1437CF	315	642	-27.6	.2C79+C1	.2949-11	-6656-
녛	£21	273	-22.1	1955+01	*2769*23	-6666-
E . I U # I	227	930	14000	10+9161.	.2539+11	0000

(0E6 C)	-9999	-6666-	-9999A	-0666-	-9999.	-6666-	-9999a	-6666-	-9999-	-6666-	-9999-	-6666-	-2888-	-6666-	-0000-	-6666-	9999	• 6666-	95555	• • • • • • • • • • • • • • • • • • • •	-6666-	-9999-	·6666-	-0666-	• 6666•	-00000	00000	6666	-9999	*6666-	-9999	-6666-	. 5666-	. 4444	-27774	• • • • • • • • • • • • • • • • • • • •	-0000		-6066-	-9999-	-6606-	-5665-	*6666-	-6666-	6666	******	-6666-
(SRAM/H3)	.2510+01	.2415+31	2104+01	.2241+61	.2175+01	.2561+01	1955-01	1879.01	1818+01	1725+01	1659+01	1596+01	1520+01	.1459+01	1413+01	.1379.01	1327401	. 2266+51	1211+61	10.6/11.	10.44.01	1022461	00+9986	9453+00	00+8506*	- 8691+0G	08528+00	2043-06	7759+06	.6942+50	.6723+90	.6583+00	-6823+0C	.6238+36	22-4609	.5837+03	2651+TL	36.545.	50.400	4903+00		25 + 55 5 4 c	*4372+SC	*136+AC	-4022+0E	1899+55	.3697+50
(MILL TRARS)	1540+01	1768+61	1699+01	.1632.01	1567+61	1505+01		1190+01	10-9226	1288+01	10.45.45.	1107401		1007+01	1055-01	.1015+01	9788400	.9368+03	. 80C6+00	.8656+00	2002-000	00.2444	.7392+00	-7109+DD	00 7289	20+6259	.6327+00	20.2.00	10+0#8.* 10+00#8.*	5413+00	5218+00	5020+00	##20aCE	00.4894.	-14464+OC	00×16ca*	-1 23+CC	.3951+03	30000000 44.00000	C C + P C V P -	1166+00	1230+00	+31r3+0a	*2975+CC	-2988+CC	2746+63	230455
1056		=18.2	2001:	101-	-22-2	a - a - 1		-15-4		0 1 1		700	7 · · · · · · · · · · · · · · · · · · ·	-11-	-12.9	-16.9	-17.2	-15.4	m1802	-17.4	-18.2	D * C T T T	-12.7	-111.1	-10.2	-9.5	-14.7	-18-3	-13.9	2 6 -	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-7.5	-11-1	-13.6	-15.9	-17.C	2.614	-2:.2	-21.2	7077	-26.	1000	-26.2	=26-2	-25.8	-25.2	7-36-
1930	334	226	0.476	103	***	45.3	3 C C	2 4 6	5 6 6	780	0 0	565	# C	780	201	101	988	690	05.6	052	050	052	950	n 4	038	04.2	952	690	100 m	121	176	221	210	236	286	542	25C	256	262	592	212	273	265	263	25.9	25.2	35.5
00000	(FT/SEC)			250	7 1		750	N. U	3 · ·	810	057	050	ייני מאוייייייייייייייייייייייייייייייייייי	021	0.20	0.00	060	020	021	027	927	023	910	2100	025	012	033	C32	£28	02.1	10 C	770	370	200	201	240	e C	072	064	C51	L S b) () (76.5	7 4 W	057		190
AL 1.1.100£	(FT)	186500	147555	146750	000667	משכחבו	151633	: 52020	153000	154030	155530	156550	157Ccŋ	158000	159063	900091	000191	00000	16.00	165.50	166700	167300	168000		17100	172000	173000	17879	175320	176220	17700	20041		10101	1977C	. B 1 . C.	20000	10000	186630	197303	: 98553		20000	20161	ביייביים	7 4 4 6	7.8

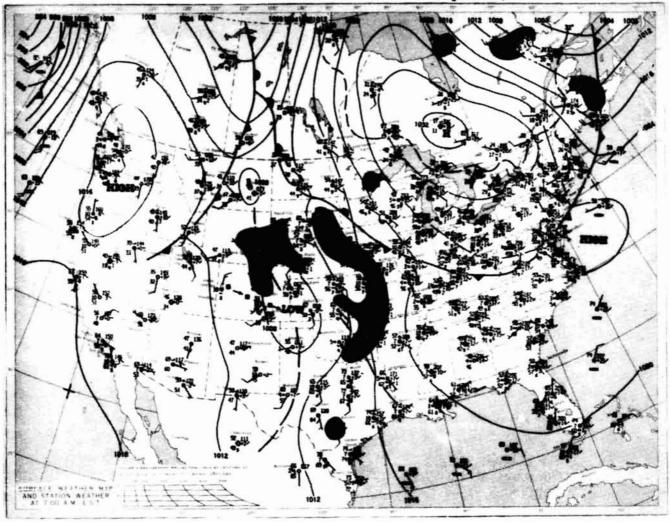
Color Colo	(MILLIBARS) -2523+00 -2433+00 -2336+00	(GPAM/M3)	(056 C)
255 255 255 255 255 255 255 255 255 255	.243400 .2433400 .2316400	-15A7+G0	
2553 2554 2554 2554 2555 2555 2555 2555	.2433400		
255 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-2316+DC	00+3640.	-0000-
25.4 26.5 27.0 29.5 29.5 29.5 29.5 29.5 20.5 20.5 20.5 20.5 20.5 20.5 20.5 20		3349+00	-6666-
256 264 264 265 265 266 266 266 266 266 266 266 266	.2239+00	.3214+90	-6666-
259 270 296 296 296 296 298 298 298 298 298 228 228 229 221 221 221 221 221 222 223 224 224 224 225 227 227 227 227 227 227 227 227 227	.2141 3	.3091+0€	-6666-
268 299 299 299 299 299 298 205 205 205 205 205 205 205 205 205 205	.2058+00	.2983+0€	-6666-
200 200 200 200 200 200 200 200 200 200	1972+DD	A2893+C3	-4666-
285 285 296 296 297 298 298 298 228 228 228 228 228 228 228	1889+00	.2796+90	-6666-
285 299 299 299 299 299 282 282 223 223 223 223 224 224 225 223 223 223 223 223 223 223 223 223	.18D9+DD	-2702±00	-6666
29.5 29.9 29.9 29.9 29.9 29.9 20.9 20.9 20.9	.1732+00	.2601+05	-9999.
296 299 299 299 298 200 200 200 200 200 200 200 200 200 20	.1657+00	,2519+00	-6656-
299 299 299 298 288 288 288 289 223 224 224 224 224 225 227 227 227 227 227 227 227 227 227	.1584+00	-2439+0C	-6666-
299 299 292 292 282 256 241 221 221 221 221 222 223 223 223 223 22	1514+00	,2355+50	-6666-
298 298 298 282 282 284 285 284 223 223 223 223 223 223 223 223 223 22	1.446+00	.2254+00	-6666-
298 292 282 282 256 256 256 223 224 224 227 227 227 227 227 227 227 227	1382+00	2159+00	-0000-
292 288 2182 202 203 203 203 203 203 203 203 203 20	1320+00	2071+60	-6666-
2882 2882 2882 2884 2584 2384 2284 227 227 227 227 227 227 227 227 227 22	.1260+00	-19A7+DE	0000-
282 268 268 268 259 241 221 221 221 221 221 231 231 231 231 23	1204+00	1912+00	-0000-
282 268 258 259 241 241 221 221 221 221 221 221 221 237 244 253 253 253 253 253 253 253 253 253 253			0000
268 268 250 281 234 228 221 221 221 221 237 237 244 253 253 253 253 253 253 253 253 253 253	00+9601	1759+00	- 6666-
268 250 284 234 228 227 227 227 237 237 253 262 262 262 350 350	00+4501		0000
250 284 234 234 228 227 227 227 227 237 244 253 253 250 350 350	.9980-01	1615+00	.6666-
250 284 228 228 221 221 221 227 227 237 237 244 253 253 262 271 271 271 271 271 273 273 273 273 273 273 273 273 273 273	49510+01	.1548+0G	-9999
241 234 228 221 221 221 221 221 231 244 253 253 271 271 271 271 271 271 271 271 271 271	.9070-01	.1483+00	-6666-
234 228 221 221 221 221 227 237 244 253 262 271 271 271 271 271 271 271 271 271 27	.8650-01	1821+55	-9999
228 221 221 221 221 227 227 237 244 262 262 262 271 271 271 271 271 271 271 271 271 27	.8240-01	.1354+00	-6666-
224 221 221 221 221 221 231 242 252 262 271 271 271 271 271 271 271 271 271 27	.7863-01	.1292+0€	* 6666 -
221 221 221 221 227 231 232 262 262 271 271 271 271 271 271 271 271 271 27	.7500-01	.1232+00	-6666-
221 221 221 227 227 237 253 262 271 271 271 272 287 287 287 287 287 287 287 289 289 280 300 300	.7150-61	.1175+05	-6666-
221 221 223 224 234 244 253 262 271 271 271 272 273 263 353 353	.6820-01	.1121+00	-0666-
221 227 231 231 244 253 271 271 271 271 271 271 271 271 271 271	13-06#9*	1269+DC	-9999a
227 231 231 244 253 262 271 271 271 271 271 271 271 271 271 27	.6180-01	.1020+00	-6666-
227 234 244 253 262 271 271 271 287 294 305	.5A73-01	-9760-n1	-0000-
231 244 244 253 262 271 287 284 353 353	.559Q-01	.9407-01	060 6-
237 264 262 262 271 271 287 284 300 300 300 300	-5320-D1	-9087-01	5666-
25.3 26.2 27.1 27.1 28.7 28.4 30.0 30.0 30.0 30.0	10-0905	.8730-01	6666
25.3 26.2 27.1 21.9 28.7 28.0 30.0 30.0 30.0	4.520-01	-8421-11	-6666 -
262 271 272 287 284 303 303 309		TO-66DB*	* 6666=
271 219 284 284 363 363 369	10-237 5	1756-71	-4444
219 287 294 350 105 309	10-0214	1422-01	6666-
287 294 350 350 309	16-0161	.7558-01	-6666-
350 350 309 309	.3716-01	.6738-01	• 6666-
30.0 30.9 30.9	.3525-51	10-45494	-6666-
329	.334C+01	.6189-01	* 6667-
Ф С П - М -	1166-51	12-1165	-9999-
C-1	.2990-01	.5633-01	-6666-
	.2835-51	.5358-C1	-6865-
316	.2680-01	.5102-01	-6666-
118 126	.2543-01	A 4 5 5 8 - 11 1	-6666-

ALTITUDE	WIND SPEED	MIND DIRECTION	TEMPERATURE	PDFSSIIDE	DFRATTA	TATO DIE
(FT)	(FT/SEC)	_	(056 5)	(MILL TRABS)	(10.00
286950	121	12.1	1.00-	.2270=01	4774-03	0000
247030	133	325	-90.2	.2156-31	10-1004	-0000
248000	133	128	-90.2	2030-01	10 11 10 11	0000
24900		120	=00.2	10-10-1	170	-00-
250000	133	33.1	1000	10-02/11	1010000	0000
251000	128	eri eri	4.04	1725-63	7255	-0000
25,2000	121	444) () (# C (9 d C P	00000
253000	119	117	4.84	.0-0	1036-31	-2222
254000	3				TD 192620	• * * * * * * * * * * * * * * * * * * *
255-00	178	74.1	2 7 8 -	- C - C - C - C - C - C - C - C - C - C	2606 01	24444
256369		4 F			10+64:30	* 6666
25,200	700	***	7000	10=01614	17.675	-6666-
	7.00	0 i	7.09	10-0-21	10-8622*	-6666-
25.002	186	19.7	=BusC	1180-01	.2173-01	-6666-
22005	910	325	-83.2	.1120-01	.2054-01	-6666-
260530	065	353	-81.9	1060-01	1931-01	-0666-
261JCC	CSS	358	-8 J. 4	×1010-01	.1825-01	-9990-
262350	043	003	*80.2	9650=02	1733-01	0000-
263000	033	012	-79.3	010000	1616-01	0000=
264000	023	528	_78.P	5 C = 0.0 + 0 -	1542-01	0000
265600	016	061	-78.2	-8200-02	.1465-01	-0000-
266030	<u> </u> <u> </u>	10.6	-78.2	1850-02	10-10-1	0000
267033	028	132	-77-2	-7400-02	.1316-01	-9999
26,600	0.18	14.5	-17.2	-7acn-n2	1249-01	0006-
269030	052	153	-77.2	-6600-02	-1173-91	6666-
270000	590	158	-76-2	-6 300-02	1114-01	-6666-
271000	679	162	-76.2	.6000-62	.1061-01	-6666-
272030	092	166	-74.6	5700-02	1000-01	*0000=
273C ₃ r	176	169	-73.2	.5400-02	9406-02	-9999-
274900	119	172	-72.5	.51ca-02	6858-02	0000-
275600	112	173	-73.C	20-4064	.8517-02	-6666-
276055	105	175	-72.4	4715-02	8189-92	6666-
277066	098	177	-73.9	4534-02	.7875-02	-6666-
278050	196	180	-74.3	4360-02	1572-52	-0000-
279000	G8 5	182	-14.1	.4192-32	.7281-32	-6666-
280000	078	186	-75.1	-4631-92	1001-92	-9999
281700	270	189	-15.6	.3876-02	.6731-72	-6666-
292020	0.66	194	-16.5	3727-02	■ 6472-02	-6666-
2837C?	T 5 2	199	-76.4	.3583-C2	.6223-52	6606-
4	057	256	5-47=.	3445-02	559B4-32	6666-
285333	523	213	-77.3	.3313-02	5754-35	6666-
286003		221	-772-7	.3186-62	. 5533-C2	6656-
287000	かれび	230	-78.1	.3063-02	.5323-C2	• 6666-
286555	C4.8	239		-2945-62	5115-52	-6666-
289037	9 a C	8 \$11	-79.	.2832-52	26-6164*	-6666-
-92525	350	254		2425-02	4357-02	46566-
1050C	250	259	-79.5	.2077-02	3735-22	6660-
296320	124			.1735-02	3172-22	6666-
351750	167	267	-74.9	•153è-E2	+2588-TE	6666-
3G#07F	231	268	2.5	1317-52	2279-72	-6666-
30700	291	269	-72.1	1124-62	101010	0.00

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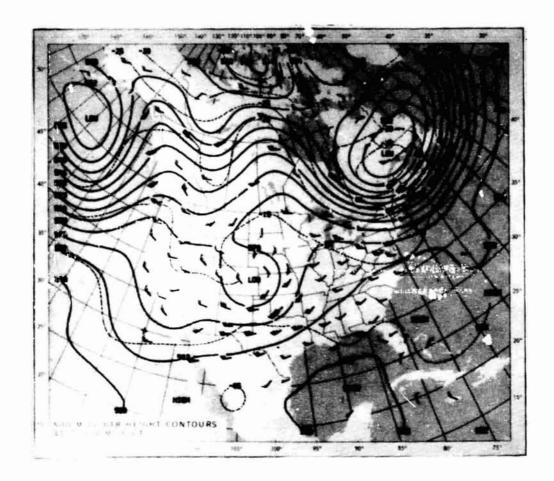
TITUDE	MIND SPEED	MIND DIRECTION	IE NPERATURE	PRES SURE	DENSITY	DEN POINT
	(FT/SEC)	(0EG)	(DEG C)	(MILLIBARS)	(GRAM/M3)	(DEG C)
110050	134	269	-70s	9459=01	1618-02	-0000-
313000	36.0	269	-69.1	.8279-03	-1390-02	-6666-
114000	369	269	-67.5	.7104-03	1181-02	-9999-
	378	269	0.99-	.6095-03	1003-02	-6666-
12220	363	269	4-49-	.5229-03	.8522-03	₹6666
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9	295	269	-6102	. 3849-C3	.6151-03	-9999
331000	301	269	-56.8	.3296-03	.5200-03	-6666-
334000	301	269	=56.5	2826-03	.4396-03	*6666=
ç	291	269	-54.1	.2422-03	.3716-03	-6666-
34000	267	240	-51.7	2075-03	.3141-03	-6666-
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366030	195	269	## fa.2	1531-63	,2251-D3	-9999.
349000	190	268	-42.5	1327-03	NU-1161.	-6666-
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355000		267	-35.0	*0-53-66*	.1381-03	-6666-
15.2000	110	264	-31.43	8620-08	1176-03	-6666-
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367000	4:0	25.7	-15.3	*0-9065*	.7*85-54	-6666-
370000	042	24.8	-6-	.5248-04	-6473-G4	-6666-
E	029	226	-3.D	*4660-04	*S599-54	-6666-
176,000	026	17.2	3.2	-4136-D4	46-2484	6666
379000	025	129	10.3	.3712-04	.4222-04	•6666-
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38800	026	137	35.7	2802=04	.2899-D#	-6666-
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	345	71	72.5	20-4-06	1830-04	0000=

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Surface Synoptic Map at 1200 UT October 5, 1984 — Isobaric, Frontal, and Precipitation Patterns are Shown in Standard Symbolic Form.

Figure 1. Surface synoptic chart 57 min after launch of STS-41G.



500 Millibar Height
Contours at 1200 UT
October 5, 1984.
Continuous Lines Indicate Height Contours in Feet Above
Sea Level. Dashed Lines are Isotherms in Degrees Centigrade. Arrows Show Wind Direction and Speed at the
500 MB Level.

Figure 2. 500 mb map 57 min after launch of STS-41G.

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CLOUD PHOTOGRAPH NOT AVAILABLE

1.00 100 140

Figure 3. GOES-5 visible imagery of cloud cover 3 min prior to launch of STS-41G (1100 UT, October 5, 1984). 500-mb contours and wind barbs are also included for 1200 UT.

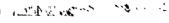
CLOUD PHOTOGRAPH NOT AVAILABLE

Figure 4. Enlarged view of GOES-5 visible imagery of cloud cover taken 3 min prior to launch of STS-41G (1100 UT, October 5, 1984). Surface temperatures and wind barbs for 1100 UT are also included.

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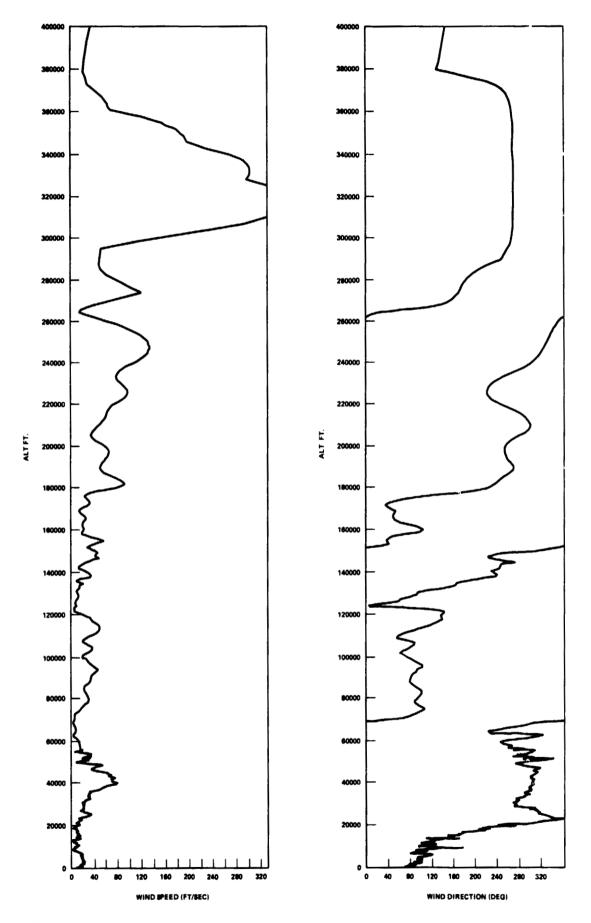


Figure 5. Scalar win? speed and direction at launch time of STS-41G.

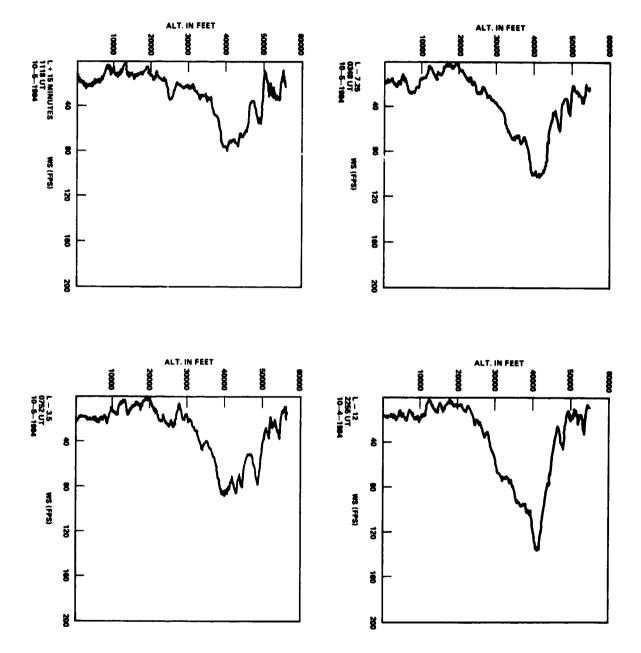
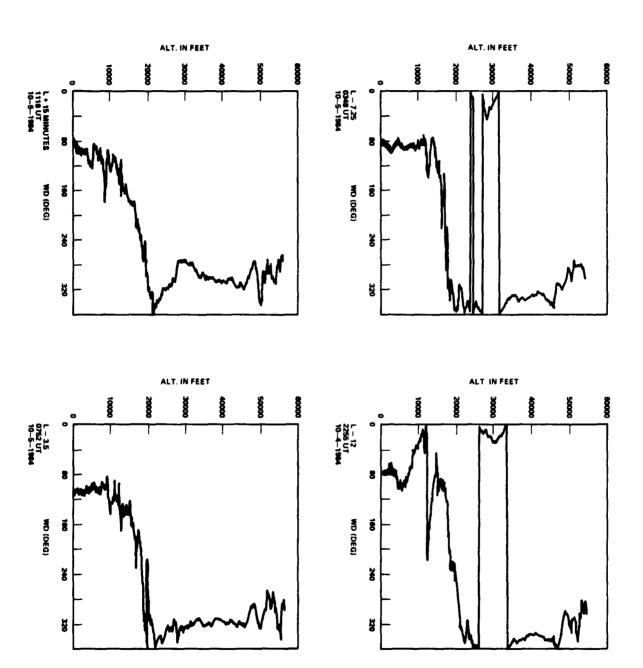


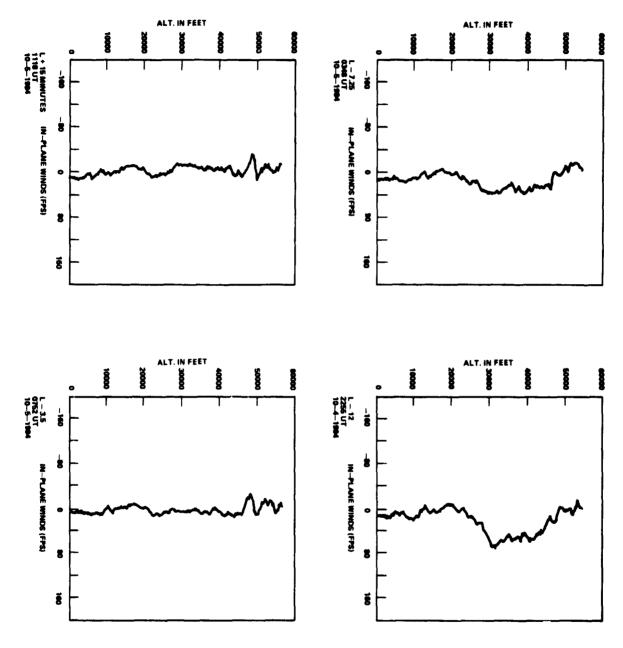
Figure 6. STS-41G prelaunch/launch Jimsphere-measured wind speeds (FPS).



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Figure 7. STS-41G prelaunch/launch Jimsphere-measured wind directions (degrees).



STS-41G prelaunch/launch Jimsphere-measured in-plane component winds (FPS). Flight azimuth = 39 degrees. Figure 8.

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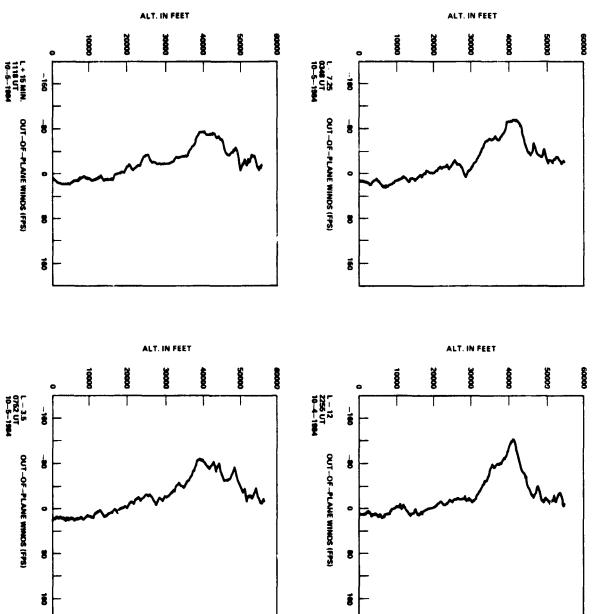


Figure 9. STS-41G prelaunch/launch Jimsphere-measured out-of-plane components winds (FPS). Flight azimuth = 39 degrees.

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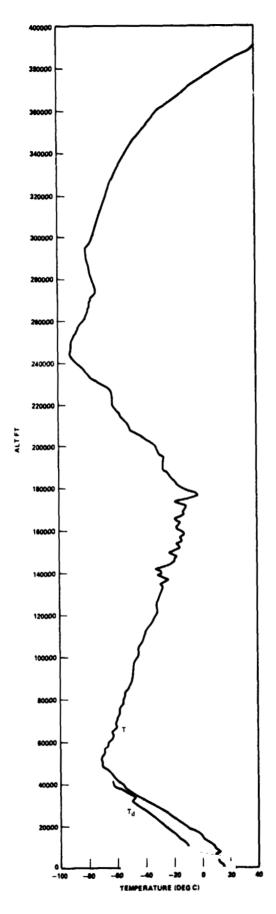


Figure 10. STS-41G temperature profiles versus altitude for launch (ascent).

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APPROVAL

ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-41G) LAUNCH

By D. L. Johnson, C. K. Hill, G. Jasper, and G. W. Batts

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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